

# Optimizing a CIGS Thin-Film Solar Cell with SILVACO ATLAS: Effects of Optical Bandgap and Absorber Electron Affinity

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## Abstract

This study uses TCAD numerical simulation to evaluate how key absorber parameters in Cu(In, Ga)Se<sub>2</sub> (CIGS) thin-film solar cells influence device performance, with the objective of identifying low-material, cost-effective optimization strategies. While crystalline-silicon (c-Si) still dominates the market despite its indirect bandgap and the thick wafers it requires, the CIGS pathway, featuring a direct, composition-tunable bandgap and a high absorption coefficient, on glass or flexible polymer substrates, offers a compelling alternative. The device investigated adopts the stack Al/ZnO/CdS/CIGS/Mo/PET and is simulated in SILVACO ATLAS (drift-diffusion transport coupled to Poisson and carrier-continuity equations) under conditions close to STC (AM1.5G, 27°C, 1000 W·m<sup>-2</sup>). Parameter sweeps cover the absorber optical bandgap  $g \in [1.14, 1.50]$  eV, electron affinity  $\chi \in [4.0, 4.8]$  eV, and CIGS thickness  $d \in [0.1, 3.0]$  μm, with p-type doping fixed at  $1 \times 10^{16}$  cm<sup>-3</sup>. The results show that the short-circuit current density  $J_{sc}$  is nearly invariant with respect to  $E_g$  and  $\chi$  once the absorber is sufficiently thick ( $d \geq 0.3$  μm); a deviation appears at  $d = 0.1$  μm, attributed to stronger optical losses (residual transmission) and less efficient carrier collection. In contrast, the open-circuit voltage  $V_{oc}$  increases markedly with  $E_g$  over the investigated range (consistent with a reduced effective saturation current), which in turn raises the fill factor  $FF$  and the power-conversion efficiency  $\eta$ . The electron affinity  $\chi$  has little influence on  $J_{sc}$  (except for  $d < 0.3$  μm), but it systematically impacts  $V_{oc}$ ,  $FF$ , and  $\eta$  via band alignment at the buffer/absorber interface. Within our parameter window, a maximum efficiency of about

27.05% is achieved for  $E_g \approx 1.50$  eV with  $d = 3.0$   $\mu\text{m}$ , where gains in  $V_{oc}$  and  $FF$  compensate the near-invariance of  $J_{sc}$ . Moreover, electron-affinity windows of  $\chi \approx 4.0 - 4.2$  eV and  $\chi \approx 4.6 - 4.8$  eV are shown to be favorable across  $0.1 - 3.0$   $\mu\text{m}$ . These findings suggest that joint engineering of composition (Ga content) to tailor  $E_g$  and of band alignment (through  $\chi$  and the CdS/CIGS/ZnO interfaces) is a robust route to boost CIGS efficiency while minimizing material usage.

## Keywords

CIGS Thin-Film Solar Cells, Optical Bandgap, Electron Affinity, Band Alignment (CdS/CIGS), Open-Circuit Voltage, Fill Factor, Power-Conversion Efficiency

## 1. Introduction

The global photovoltaic market remains largely dominated by crystalline-silicon (c-Si) solar cells, a mature, industrialized technology known for reliability, high field efficiencies, and long service lifetimes. Silicon is abundant, low-toxicity, and low-cost, and it can be readily doped with boron or phosphorus. Nevertheless, intrinsic limitations, an indirect bandgap ( $E_g \approx 1.12$  eV) and a low absorption coefficient ( $\sim 104$   $\text{cm}^{-1}$ ), necessitate thick wafers ( $\geq 100$   $\mu\text{m}$ ) to efficiently absorb the solar spectrum, which raises material and energy consumption and, ultimately, costs [1].

These constraints have fueled growing interest in thin-film technologies, which aim to reduce material usage and manufacturing costs while maintaining competitive performance [2]. Among them, Cu(In, Ga)Se<sub>2</sub> (CIGS) stands out for its high absorption coefficient and direct, composition-tunable bandgap ( $\approx 1.04 - 1.68$  eV with gallium content), as well as its compatibility with diverse substrates (glass, flexible polymers) and multiple deposition routes (co-evaporation, sputtering, PLD, screen printing), enabling flexible and Cd-free architectures [2]-[6]. These attributes motivate the performance optimization of CIGS thin-film devices, the focus of the present study.

The objective here is to quantify the influence of two key absorber parameters, the optical bandgap  $E_g$  and the electron affinity  $\chi$ , on the main figures of merit: short-circuit current density  $J_{sc}$ , open-circuit voltage  $V_{oc}$ , fill factor  $FF$ , and power-conversion efficiency  $\eta$ . To this end, we numerically simulate a laboratory-grade CIGS device using TCAD SILVACO-ATLAS, solving Poisson and carrier-continuity equations coupled through the drift-diffusion transport model [3] [7] [8].

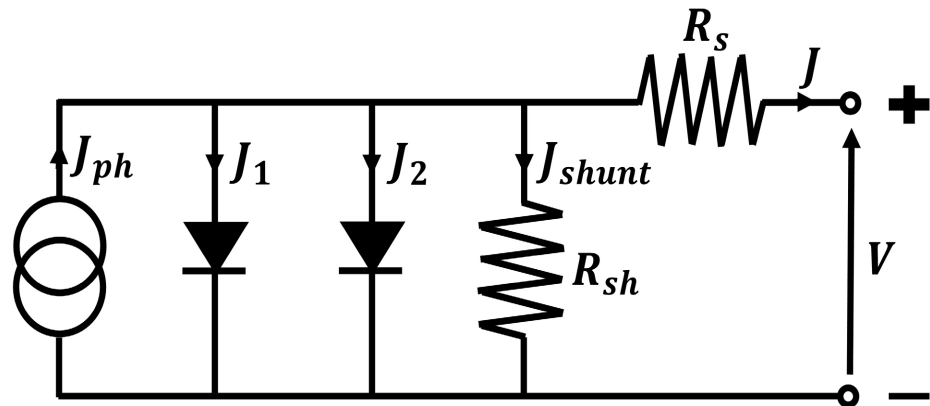
The paper is organized as follows. Section 2 revisits the electrical modeling and the characteristic parameters of CIGS cells (equivalent circuit,  $J(V)$  relation,  $J_{sc}$ ,  $V_{oc}$ ,  $FF$ , and  $\eta$ ). Section 3 details the materials, device structure, method,

and simulation settings. Section 4 presents the results, followed by their analysis and discussion.

## 2. Modeling and Electrical Parameters of CIGS Thin-Film Solar Cells

### 2.1. Equivalent Electrical Circuit

A CIGS solar cell is a p-n heterojunction (p-type CIGS absorber, n-type buffer layer, and TCO window). Its electrical behavior is classically modeled by a two-diode equivalent circuit comprising a photogenerated current source ( $J_{ph}$ ), a series resistance ( $R_s$ ), and a shunt resistance ( $R_{sh}$ ), as shown in **Figure 1** [9] [10].



**Figure 1.** Equivalent electrical circuit of a CIGS thin-film solar cell.

In this framework,  $R_s$  aggregates ohmic losses due to the sheet resistance of the transparent conducting oxide (i-ZnO/ZnO:Al), interfacial resistances, the back contact (Mo/CIGS), and the bulk resistivity of the active layers, whereas  $R_{sh}$  accounts for leakage currents that partially short the junction (pinholes, percolation along grain boundaries, deep defects, metallic impurities) [9] [11]. The two diodes represent distinct recombination pathways (space-charge region vs. quasi-neutral regions), which enables faithful reproduction of the dark and illuminated  $J$ - $V$  characteristics and of the impact of  $R_s$  and  $R_{sh}$  on the fill factor ( $FF$ ) and the power conversion efficiency (PCE) [8]-[10].

### 2.2. Electrical Parameters

#### 2.2.1. Current Density-Voltage Characteristic $J(V)$

The current density delivered by a CIGS thin-film solar cell under load, within the two-diode model, is written as:

$$J = J_{ph} - J_{01} \left\{ \exp \left[ \frac{q(V + R_s J)}{n_1 k_B T} \right] - 1 \right\} - J_{02} \left\{ \exp \left[ \frac{q(V + R_s J)}{n_2 k_B T} \right] - 1 \right\} - \frac{V + R_s J}{R_{sh}} \quad (1)$$

where  $J_{01}$  and  $J_{02}$  are the saturation current densities ( $\text{A}\cdot\text{cm}^{-2}$ ),  $n_1$  and  $n_2$  are the diode ideality factors,  $R_s$  and  $R_{sh}$  are the (area-normalized) series and shunt resistances ( $\Omega\cdot\text{cm}^2$ ),  $J$  is the current density ( $\text{A}\cdot\text{cm}^{-2}$ ),  $q$  the elementary charge (C),  $k_B$  the Boltzmann constant ( $\text{J}\cdot\text{K}^{-1}$ ),  $T$  the temperature (K),  $V$  the terminal voltage, and  $J_{ph}$  the photogenerated current density ( $\text{A}\cdot\text{cm}^{-2}$ ) [11]. The  $J$ - $V$  characteristic is measured under standard test conditions (STC), typically AM1.5G spectrum,  $T = 25^\circ\text{C}$ , and irradiance  $G = 1000 \text{ W}\cdot\text{m}^{-2}$  [12].

### 2.2.2. Short-Circuit Current Density $J_{sc}$

The short-circuit current density, measured at  $V = 0$ , ideally equals the photocurrent ( $J_{sc} \approx J_{ph}$ ). It depends on irradiance and spectrum, optical absorption and reflection, device thickness/quality, and minority-carrier diffusion lengths. A general expression is:

$$J_{sc} = q \int_0^{\lambda_g} I_o(\lambda) \frac{\lambda}{hc} EQE(\lambda) d\lambda \approx q \int_0^{\lambda_g} I_o(\lambda) \frac{\lambda}{hc} d\lambda \quad (\text{if } EQE \approx 1) \quad (2)$$

where  $I_o(\lambda)$  is the spectral irradiance ( $\text{W}\cdot\text{cm}^{-2}\cdot\text{nm}^{-1}$ ),  $h$  is Planck's constant ( $\text{J}\cdot\text{s}$ ),  $c$  is the speed of light in vacuum ( $\text{m}\cdot\text{s}^{-1}$ ),  $\lambda$  is the wavelength (m), and  $\lambda_g$  is the cutoff wavelength associated with the absorber's optical bandgap [11].

Here  $EQE(\lambda)$  is the external quantum efficiency (electrons collected per incident photon;  $0 \leq EQE \leq 1$ ), *i.e.*, the fraction of incident photons at wavelength  $\lambda$  that generate carriers collected at the external circuit.

In (2), we assume  $EQE(\lambda) \approx 1$  and negligible front-side reflection  $R_{front}(\lambda) \approx 0$ . This first-order simplification is reasonable for an optically optimized device (e.g., low-reflectance TCO window with an anti-reflective coating and/or surface texturing), for which nearly all above-bandgap photons generate carriers that are actually collected. Formally, writing  $EQE(\lambda) = IQE(\lambda)[1 - R_{front}(\lambda)]A(\lambda)$  we adopt the upper-bound approximation  $IQE \rightarrow 1$ ,  $R_{front} \rightarrow 0$ , and  $A(\lambda) \rightarrow 1$  for  $\lambda < \lambda_g$ .

Where:

$IQE(\lambda)$ : the internal quantum efficiency,

$R_{front}(\lambda)$ : the front-side spectral reflectance,

$A(\lambda)$ : the spectral absorptance of the device,

$\lambda_g$ : the bandgap wavelength of the absorber.

### 2.2.3. Open-Circuit Voltage $V_{oc}$

At open circuit,  $J = 0$ . In the single-diode effective approximation one obtains:

$$V_{oc} = \frac{nk_B T}{q} \cdot \ln \left( \frac{J_{sc}}{J_o} + 1 \right) \quad (3)$$

where  $n$  is the (effective) ideality factor, typically  $1 \leq n \leq 2$  [13].

### 2.2.4. Fill Factor (FF)

The fill factor is defined by

$$FF = \frac{P_m}{J_{sc} V_{oc}} = \frac{J_m V_m}{J_{sc} V_{oc}} \quad (4)$$

with  $(J_m, V_m)$  the current density and voltage at the maximum-power point. The fill factor can be written as:

$$FF = FF_{id} \cdot \left( 1 - \frac{V_{oc}}{R_{sh} J_{sc}} - \frac{J_{sc} R_s}{V_{oc}} + \frac{R_s}{R_{sh}} \right) \quad (5)$$

where  $FF_{id}$  is the ideal fill factor of the cell [11] [12].

### 2.2.5. Power-Conversion Efficiency

The efficiency is the ratio of the maximum electrical power density to the incident optical power density:

$$\eta = \frac{P_m}{P_{in}} = \frac{J_{sc} V_{oc} FF}{P_{in}} \quad (6)$$

where  $P_{in}$  is the incident irradiance (e.g.,  $100 \text{ mW} \cdot \text{cm}^{-2}$  under STC) [11] [14].

## 3. Numerical Simulation

### 3.1. Materials, Structure, and Method

#### 3.1.1. Materials

The thin-film solar cell under study consists of a polyethylene terephthalate (PET) substrate, a molybdenum (Mo) back contact, a Cu(In, Ga)Se<sub>2</sub> (CIGS) absorber, a CdS buffer layer, a ZnO window (transparent conducting oxide, TCO), and two aluminum metal fingers deposited on the TCO to collect the front-side current [3] [4] [15].

#### 3.1.2. Structure

The stack is Al/ZnO/CdS/CIGS/Mo/PET, in a substrate configuration (front-side illumination through the TCO window and Al grid). The structural schematic is shown in **Figure 2** [3] [5] [16].

#### 3.1.3. Method

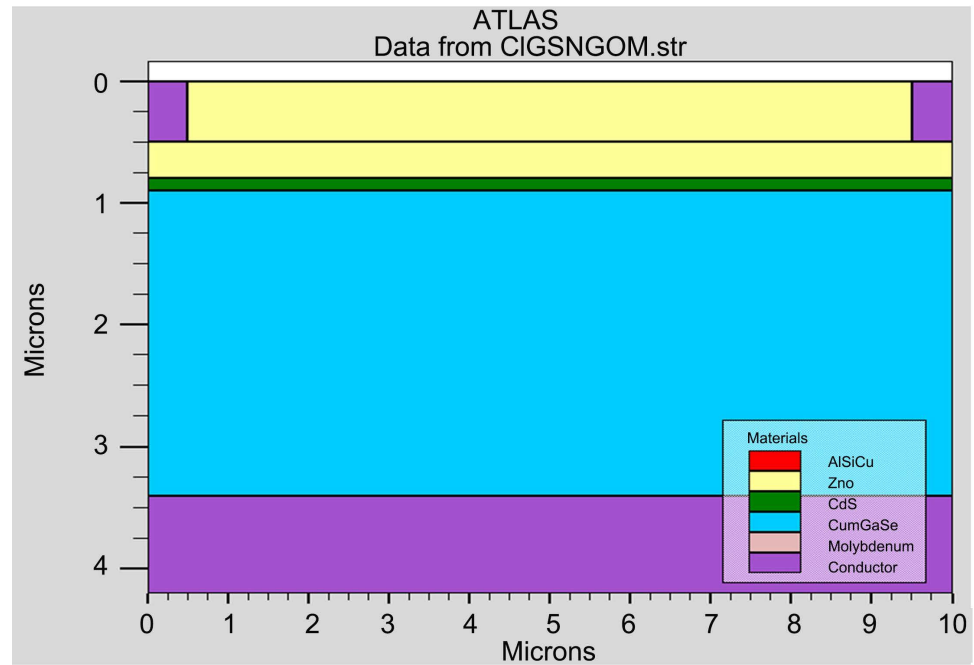
We investigate, by numerical simulation, the influence of two key absorber parameters, optical bandgap  $E_g$  and electron affinity  $\chi$  on the photovoltaic figures of merit (short-circuit current density  $J_{sc}$ , open-circuit voltage  $V_{oc}$ , fill factor  $FF$ , and efficiency  $\eta$ ). Calculations are performed using SILVACO ATLAS, by solving Poisson's equation and the carrier continuity equations coupled with the drift-diffusion transport model [7] [8].

#### 3.1.4. Simulation Parameters

Layer thicknesses follow the reference device specifications from our laboratory when available; the remaining parameters are taken from the literature [3] [7] [8]. A parametric analysis is conducted over the following ranges:

- CIGS bandgap  $E_g$  from 1.14 to 1.50 eV;
- Electron affinity  $\chi$  from 4.0 to 4.8 eV;
- CIGS thickness from 0.1 to 3.0  $\mu\text{m}$ .

Unless stated otherwise, the absorber doping is fixed at  $1 \times 10^{16} \text{ cm}^{-3}$ , a value retained from our previous simulations.



**Figure 2.** Schematic of the simulated CIGS cell structure (substrate configuration).

Numerical convergence. We verified convergence by refining the mesh (halving  $\Delta x$  and  $\Delta y$  in ZnO/CdS/CIGS and near the electrodes), reducing the voltage sweep step (vstep: 20 mV  $\rightarrow$  10 mV  $\rightarrow$  5 mV), and doubling the spectral discretization (120  $\rightarrow$  240 wavelengths). Deviations in  $V_{oc}$ ,  $J_{sc}$ ,  $FF$ , and  $J_0$  remained  $<0.5\%$  (or  $<0.3 \text{ mA}\cdot\text{cm}^{-2}$  for  $J_{sc}$  and  $<0.3$  percentage point for  $FF$ ). The time per bias point reported by ATLAS ranges from 0.01 to 0.05 s with the final setup.

**Table 1** and **Table 2** present the optoelectronic and geometric parameters (**Table 1**), as well as the defect parameters in the various layers (**Table 2**).

**Table 1.** Material properties (input parameters used in the simulations).

Materials	CIGS	CdS	ZnO
Optical bandgap $E_{g300}$ (eV)	1.14 - 1.5	2.4	3.3
Thickness $d$ ( $\mu\text{m}$ )	0.1 - 3 $\mu\text{m}$	0.1	0.8
Electron affinity $\chi$ (eV)	4.0 - 4.8	4.5	4.1
Relative dielectric permittivity $\epsilon_r$	13.6	10	9
Effective electron state density $N_{C300}$ ( $\text{cm}^{-3}$ )	$2.2 \times 10^{18}$	$2.2 \times 10^{18}$	$2.2 \times 10^{18}$
Effective hole state density $N_{V300}$ ( $\text{cm}^{-3}$ )	$1.8 \times 10^{19}$	$1.8 \times 10^{19}$	$1.8 \times 10^{19}$
Electron mobility $\mu_n$ ( $\text{cm}^2\cdot\text{V}^{-1}\cdot\text{s}^{-1}$ )	100	100	100
Hole mobility $\mu_p$ ( $\text{cm}^2\cdot\text{V}^{-1}\cdot\text{s}^{-1}$ )	25	25	25
Electron lifetime $\tau_n$ (s)	$1 \times 10^{-7}$	$1 \times 10^{-7}$	$1 \times 10^{-7}$
Hole lifetime $\tau_p$ (s)	$1 \times 10^{-7}$	$1 \times 10^{-7}$	$1 \times 10^{-7}$
Acceptor concentration $N_A$ ( $\text{cm}^{-3}$ )	$6 \times 10^{16}$	-	-
Donor concentration $N_D$ ( $\text{cm}^{-3}$ )	-	$1 \times 10^{18}$	$1 \times 10^{18}$

**Table 2.** Defect properties.

Materials	CIGS	CdS	ZnO
Gaussian defect concentration ( $\text{cm}^{-3}$ )	$N_{DG} = 1. \times 10^{14}$	$N_{DA} = 1. \times 10^{15}$	$N_{DA} = 1. \times 10^{15}$
Gaussian defect concentration ( $\text{cm}^{-3}$ )	0.1	0.1	0.1
Peak energy $E_{GA}$ and $E_{GD}$ (eV)	0.6	1.2	1.65
Electron capture cross section $\sigma_n$ ( $\text{cm}^2$ )	$1. \times 10^{-17}$	$1. \times 10^{-17}$	$1. \times 10^{-17}$
Hole capture cross section $\sigma_p$ ( $\text{cm}^2$ )	$1. \times 10^{-15}$	$1. \times 10^{-15}$	$1. \times 10^{-15}$

## 4. Results and Discussion

### 4.1. Effect of the Absorber Optical Bandgap

The optical bandgap of the CIGS absorber is given by:

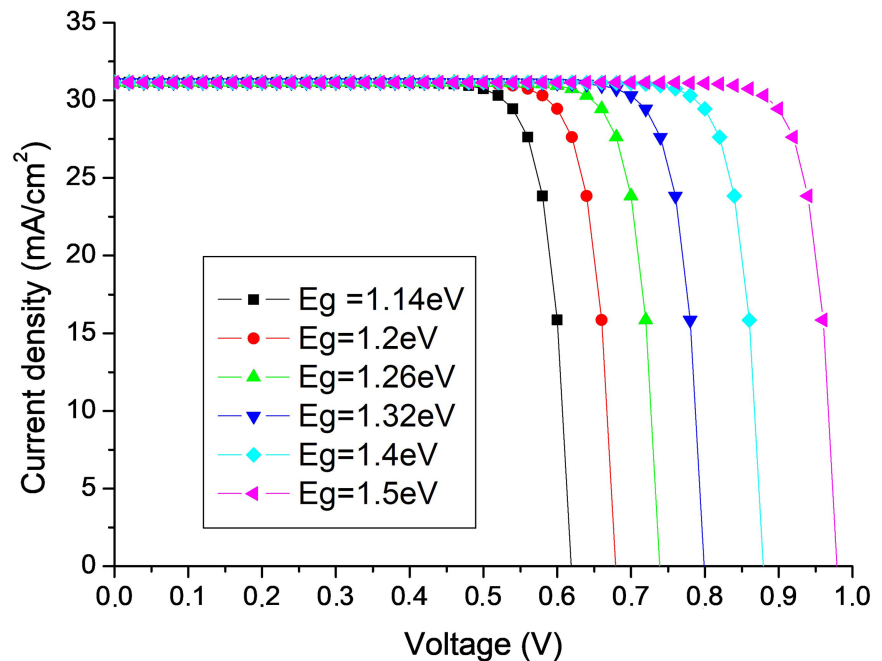
$$E_g = 1.04 + 0.64x - 0.15x(1 - x) \quad (7)$$

where  $x = \text{Ga}/(\text{In} + \text{Ga})$  is the gallium content [7].

This relation shows that the CIGS bandgap is tunable from 1.04 to 1.68 eV. By varying  $x$  from 0.2 to 0.8, we obtained bandgap values in the 1.14 - 1.50 eV range. In what follows, we analyze how  $E_g$  affects the  $J(V)$  characteristic, the short-circuit current density, the open-circuit voltage, the fill factor, and the cell efficiency.

#### 4.1.1. Effect of Absorber Bandgap on the Current-Voltage Characteristic

Figure 3 shows the current-density evolution as a function of voltage for different absorber bandgap values.

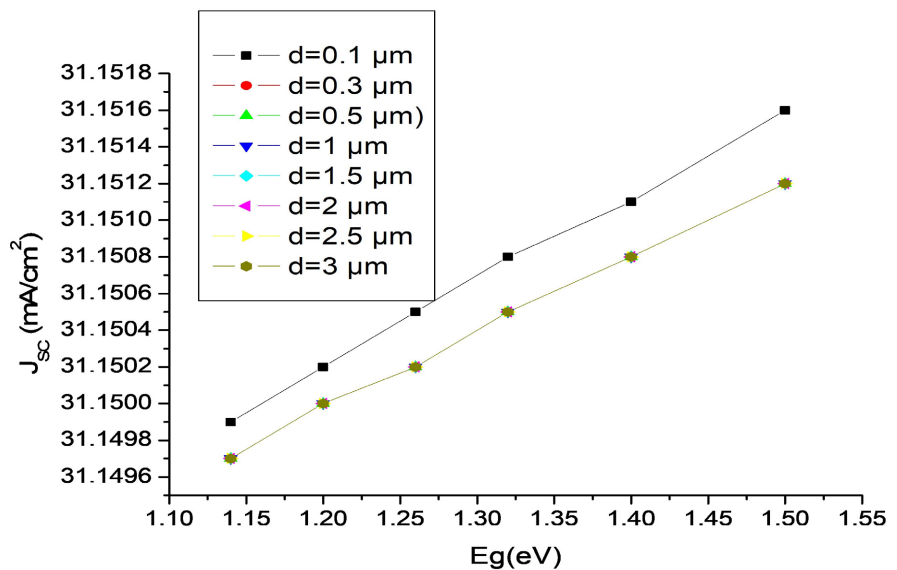


**Figure 3.** Current-density-voltage characteristics for different absorber bandgaps in CIGS.

**Figure 3** shows that all  $J$ - $V$  curves intersect the current axis at the same point ( $J_{sc} = 31.15 \text{ mA} \cdot \text{cm}^{-2}$ ), while they cross the voltage axis at different values: 0.61 V, 0.67 V, 0.73 V, 0.79 V, 0.87 V, and 0.98 V. In other words, the short-circuit current remains identical, whereas the open-circuit voltage increases with the absorber bandgap  $E_g$ . Under the present simulation conditions, the bandgap does not affect  $J_{sc}$  but raises  $V_{oc}$ , consistent with a reduced effective saturation current. To substantiate these trends, we examine the effect of  $E_g$  separately on  $J_{sc}$  and  $V_{oc}$  [17].

#### 4.1.2. Effect of Absorber Bandgap on the Short-Circuit Current

As outlined above, **Figure 4** reports  $J_{sc}$  versus  $E_g$  for several absorber thicknesses. Over our parameter range,  $J_{sc}$  is nearly invariant with  $E_g$ , with minor scatter attributable to thickness-dependent optical losses [17].

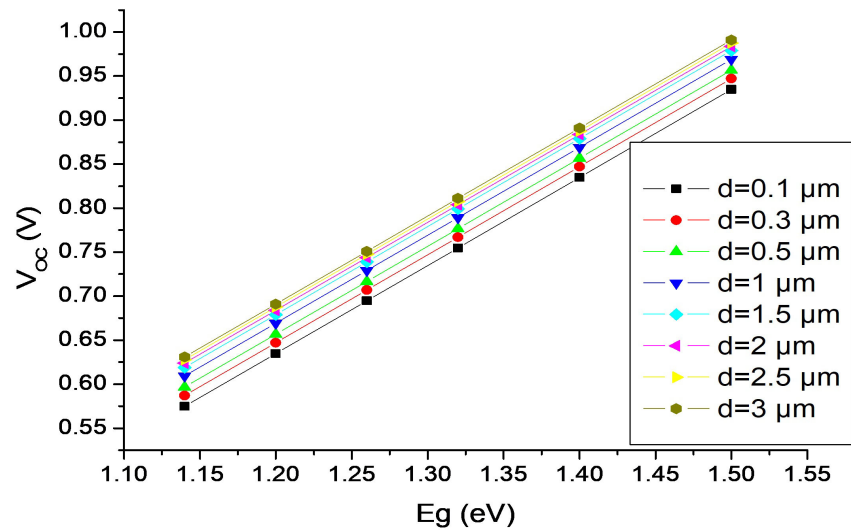


**Figure 4.** Short-circuit current density versus CIGS absorber bandgap for different thicknesses.

**Figure 4** shows that for absorber thicknesses between 0.3 and 3  $\mu\text{m}$ , the short-circuit current density remains essentially unchanged as the bandgap  $E_g$  is varied from 1.14 to 1.50 eV. In contrast, for a very thin absorber (0.1  $\mu\text{m}$ ),  $J_{sc}$  changes appreciably, indicating increased optical losses (residual transmission) in an under-thick layer. Hence, over the explored range,  $E_g$  has no significant impact on  $J_{sc}$  once the absorber is sufficiently thick, while thickness-dependent optics accounts for the deviation at 0.1  $\mu\text{m}$ . The optimum  $J_{sc}$  occurs around 0.3 - 0.5  $\mu\text{m}$ , consistent with the integral form of  $J_{sc}$  (Equation (2)) and its dependence through EQE [6].

#### 4.1.3. Effect of Absorber Bandgap on Open-Circuit Voltage

**Figure 5** shows the variation of the open-circuit voltage as a function of the optical bandgap of the absorber layer, for different thickness values.

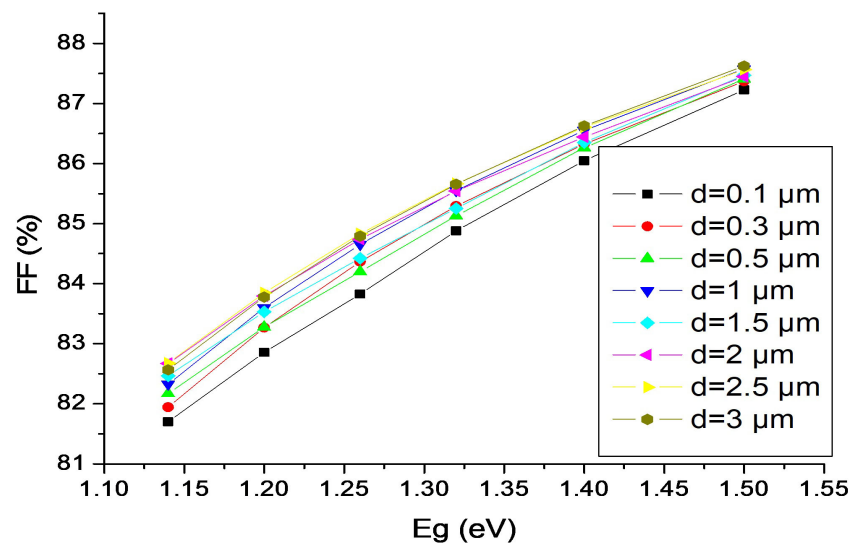


**Figure 5.** Variation of the open-circuit voltage as a function of the optical bandgap of the CIGS absorber, for different thickness values of the layer.

**Figure 5** indicates that the open-circuit voltage  $V_{oc}$  increases for all thicknesses from 0.1 to 3  $\mu\text{m}$  as  $E_g$  rises from 1.14 to 1.50 eV. This trend is attributed to the decrease in effective saturation current with wider bandgap, which, according to Equation (3), yields a larger  $V_{oc}$  [18].

#### 4.1.4. Effect of Absorber Bandgap on the Fill Factor (FF)

**Figure 6** shows the variation of the fill factor as a function of the optical bandgap of the absorber layer, for different thickness values.



**Figure 6.** Variation of the fill factor as a function of the optical bandgap of the CIGS absorber, for different absorber thickness values.

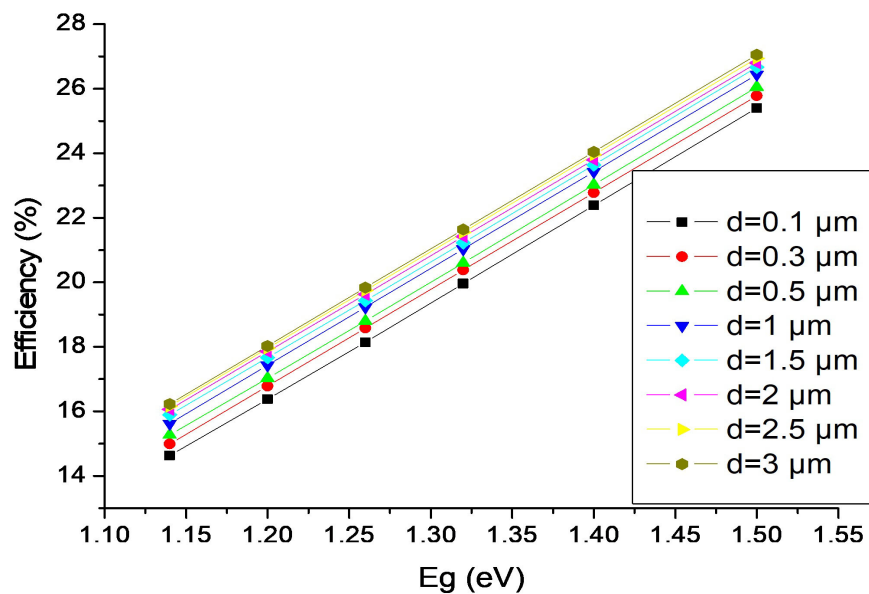
From **Figure 6**, the fill factor improves as  $E_g$  increases within 1.14 - 1.50 eV for thicknesses of 0.1 - 0.3  $\mu\text{m}$ . The rise is particularly pronounced (81.9435%  $\rightarrow$

84.3659%) at  $0.3 \mu\text{m}$  when  $E_g$  changes from 1.14 to 1.26 eV. This  $FF$  enhancement mainly reflects the dependence of  $FF_{id}$ , while first-order resistive corrections remain unchanged (Equation (4), Equation (5)).

For  $\chi_{\text{CIGS}} = 4.45 \text{ eV}$ , the saturation currents simulated under STC are  $J_0(n=1) = 1.18 \times 10^{-14} \text{ A} \cdot \text{cm}^{-2}$  and  $J_0(n=2) = 2.16 \times 10^{-8} \text{ A} \cdot \text{cm}^{-2}$ , consistent with the observed trends in  $V_{oc}$  and  $FF$ .

#### 4.1.5. Effect of Absorber Bandgap on Efficiency

**Figure 7** depicts how the optical bandgap of the CIGS absorber influences the solar cell efficiency for different values of layer thickness.



**Figure 7.** Variation of the conversion efficiency as a function of the optical bandgap of the CIGS absorber, for different absorber thickness values.

**Figure 7** shows that the efficiency  $\eta$  increases (from 14.63% to 27.05%) as  $E_g$  grows from 1.14 to 1.50 eV for thicknesses between 0.1 and  $3 \mu\text{m}$ . The gain results from stable  $J_{sc}$  (except at  $0.1 \mu\text{m}$ ) together with increasing  $V_{oc}$  and  $FF$ . Therefore, a moderate widening of the absorber bandgap can enhance CIGS device performance.

In summary, the bandgap does not significantly affect  $J_{sc}$  beyond  $0.3 \mu\text{m}$ , but it raises  $V_{oc}$ ,  $FF$ , and  $\eta$ . Targeting  $E_g \approx 1.50 \text{ eV}$  is thus a sound optimization route [19] [20].

Because optical effects (front-side reflection, residual transmission, and surface losses) are not explicitly modeled here, the integral in (2) tends to overestimate  $J_{sc}$  and, consequently, the efficiency  $\eta$ . The magnitude of this bias depends on the actual  $R_{front}(\lambda)$  and  $EQE(\lambda)$  of the device.

#### 4.2. Effect of the Absorber Electron Affinity

The electron affinity of a semiconductor is the energy required to lift an electron

from the conduction band edge to the vacuum level:

$$\chi = E_0 - E_c \quad (8)$$

where  $E_0$  is the vacuum energy and  $E_c$  the conduction-band edge.

We now examine how  $\chi$  affects the  $J(V)$  characteristic, short-circuit current, open-circuit voltage, fill factor, and efficiency.

Experimentally, the target electron-affinity range can be reached by tuning the Ga fraction  $x = \text{Ga}/(\text{Ga} + \text{In})$  during co-evaporation/three-stage selenization (Ga-grading), since for  $\text{Cu}(\text{In}_{1-x}\text{Ga}_x)\text{Se}_2$  the electron affinity follows  $\chi(x) \approx 4.61 - 1.162x + 0.034x^2$  eV, and recent work demonstrates such control via engineered Ga profiles [21] [22].

For context between 2023 and 2025, SCAPS-1D modeling studies project CIGS efficiencies above 24%, e.g., 24.43% with a p-Si BSF [23], >31% with an  $\text{Sb}_2\text{S}_3$  BSF [24], and 24.61% with a  $\text{CuAlO}_2$  BSF [25]. On the experimental side for single-junction devices, the best cells reported over the same period remain below 24% (~23% - 23.6% under STC), which underscores the value of the optimizations investigated here (increasing  $E_g$ , reducing  $J_0$ , and engineering the BSF/contacts) to bring real-world performance closer to the simulated potential.

#### 4.2.1. Effect of Electron Affinity on the Current-Voltage Characteristic

Figure 8 reports the current-density as a function of voltage for several values of the absorber  $\chi$  in CIGS.

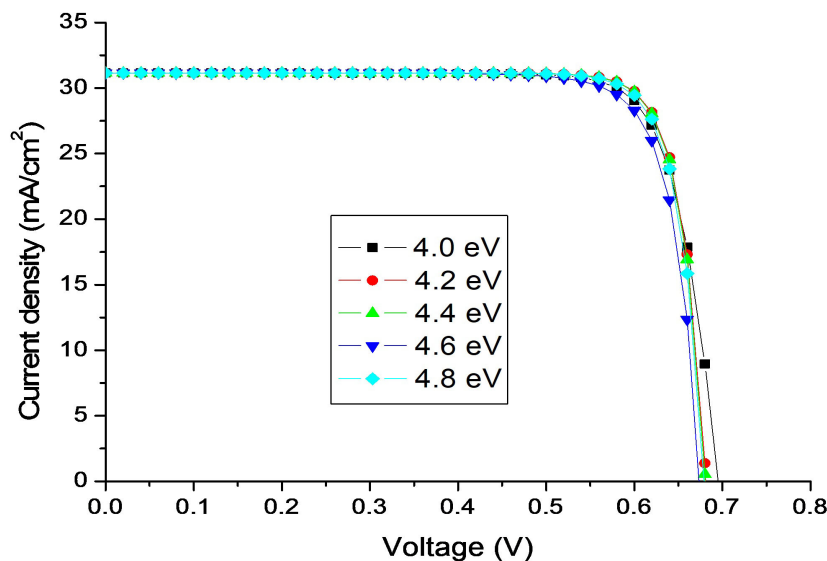


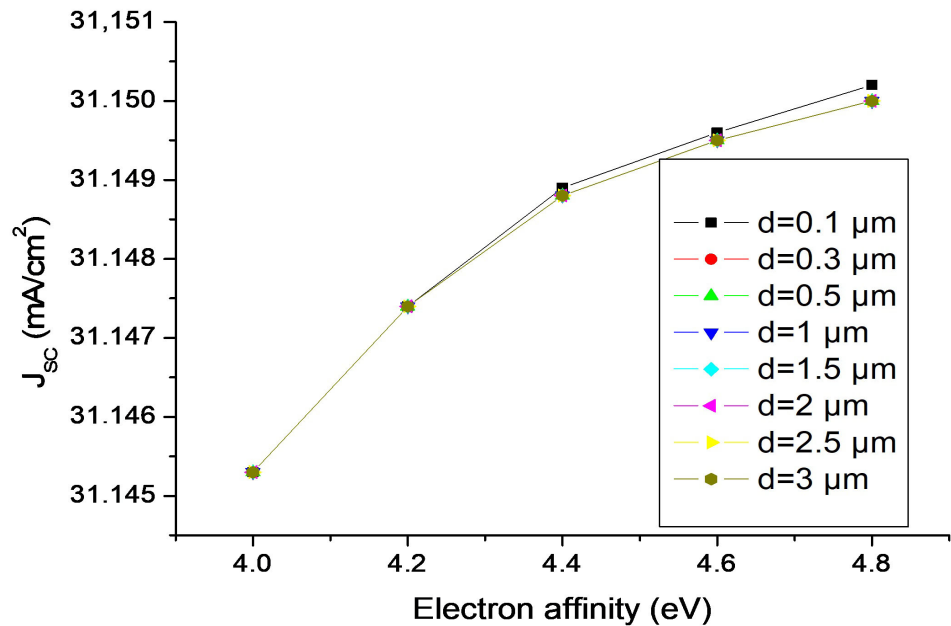
Figure 8. Current-density-voltage characteristics for different electron affinities of the CIGS absorber.

Figure 8 shows that all  $J-V$  curves intersect the current axis at the same point ( $J_{sc} = 31.15 \text{ mA} \cdot \text{cm}^{-2}$ ) as the electron affinity  $\chi$  is swept from 4.0 to 4.8 eV. In contrast, the voltage-axis intercept varies: about 0.69 V at  $\chi = 4.0$  eV, 0.68 V at  $\chi = 4.2$  or 4.4 eV, and 0.67 V at  $\chi = 4.6$  or 4.8 eV. Hence,  $\chi$  does not mate-

rially affect  $J_{sc}$  in our range, whereas  $V_{oc}$  generally decreases with increasing  $\chi$  (with a slight leveling at the upper end). To confirm these trends, we analyze  $J_{sc}$  and  $V_{oc}$  versus  $\chi$  separately [26].

#### 4.2.2. Effect of Electron Affinity on Short-Circuit Current

**Figure 9** illustrates the variation of the short-circuit current density as a function of the electron affinity of the CIGS absorber layer, for different absorber thickness values.



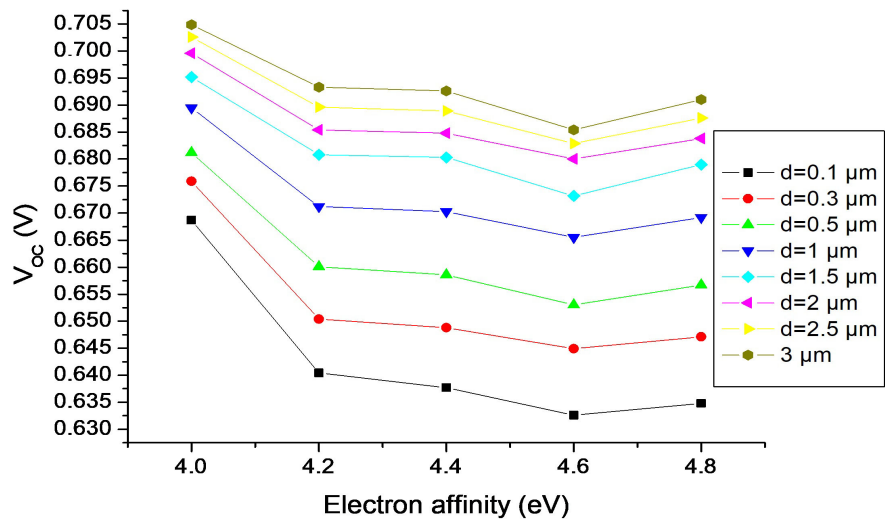
**Figure 9.** Evolution of the short-circuit current density as a function of the electron affinity of the CIGS absorber, for various thickness values.

**Figure 9** shows that  $J_{sc}$  remains unchanged for absorber thicknesses between 0.3 and 2  $\mu\text{m}$  as  $\chi$  varies from 4.0 to 4.8 eV. For a very thin absorber (0.1  $\mu\text{m}$ ),  $J_{sc}$  is constant from 4.0 to 4.2 eV, then changes as  $\chi$  increases from 4.2 to 4.8 eV. Thus, the influence of  $\chi$  on  $J_{sc}$  emerges only when the absorber is too thin (<0.3  $\mu\text{m}$ ), where band alignment and thickness-dependent optics weigh more heavily on carrier collection [9].

#### 4.2.3. Effect of Electron Affinity on Open-Circuit Voltage

**Figure 10** shows the evolution of the open-circuit voltage as a function of the electron affinity of the absorber layer, for various thickness values.

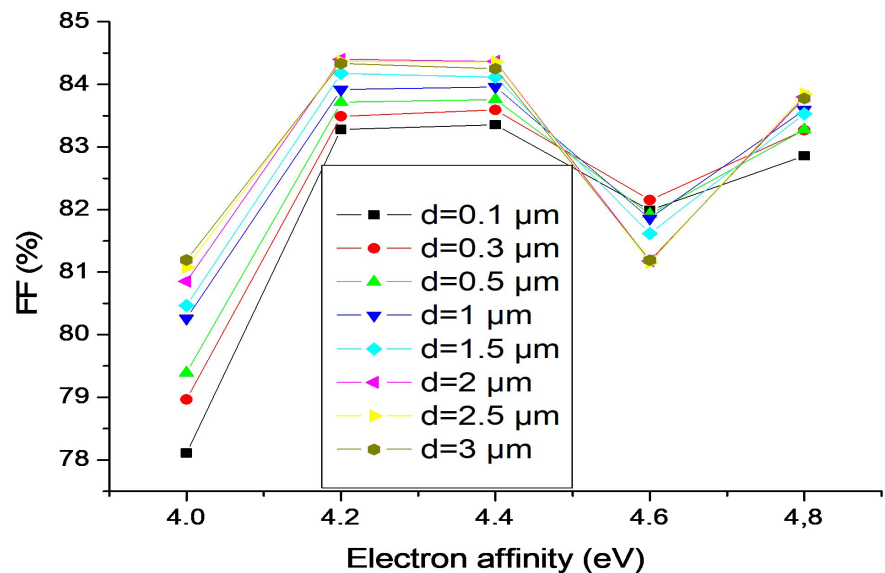
As shown in **Figure 10**,  $V_{oc}$  decreases for all thicknesses (0.1 - 3  $\mu\text{m}$ ) as  $\chi$  rises from 4.0 to 4.6 eV, followed by a slight recovery toward 4.8 eV. This behavior is consistent with an increase in effective saturation current  $J_0$  when the band alignment deteriorates (e.g., a conduction-band cliff), which reduces  $V_{oc}$  via Equation (3); when the offset approaches a more favorable regime (e.g., a small spike), interface recombination drops and  $V_{oc}$  recovers [10] [27].



**Figure 10.** Evolution of the open-circuit voltage as a function of the electron affinity of the CIGS absorber for various thickness values.

#### 4.2.4. Effect of Electron Affinity on the Fill Factor

**Figure 11** shows the variation of the fill factor as a function of the electron affinity of the absorber layer, for various thickness values.



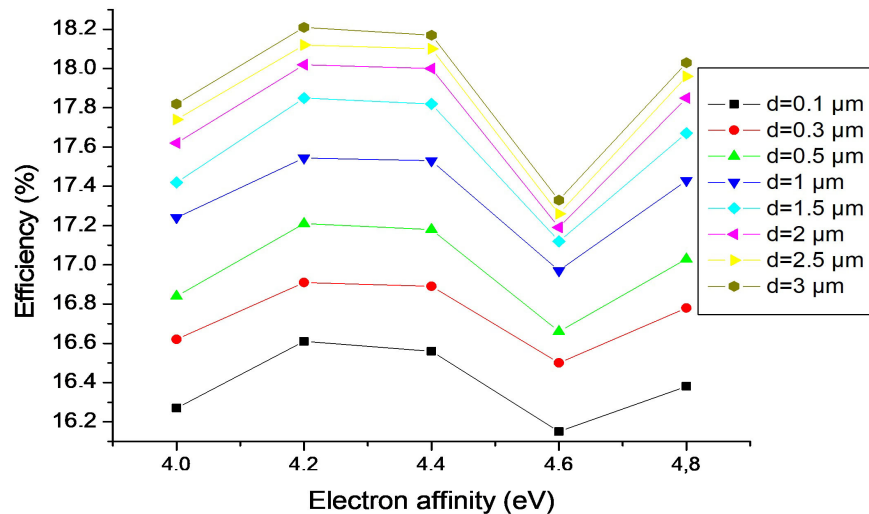
**Figure 11.** Evolution of the fill factor as a function of the electron affinity of the CIGS absorber for various thickness values.

From **Figure 11**, the fill factor improves for  $\chi$   $4.0 \rightarrow 4.2$  eV and  $4.6 \rightarrow 4.8$  eV, while it degrades within  $4.2 \rightarrow 4.6$  eV, across all thicknesses (0.1 - 3  $\mu\text{m}$ ). This response reflects the combined evolution of  $V_{oc}$  (setting  $FF_{id}$ ) and resistive losses (first-order in  $R_s$  and  $R_{sh}$ , Equation (4), Equation (5)). A less favorable offset in the 4.2 - 4.6 eV window enhances interface recombination (apparent rise of  $J_0$ ), thereby lowering  $FF$ ; near 4.0 - 4.2 and 4.6 - 4.8 eV, a better alignment

mitigates losses and raises  $FF$ .

#### 4.2.5. Effect of Electron Affinity on Efficiency

**Figure 12** shows the evolution of the conversion efficiency as a function of the electron affinity of the absorber layer, for various thickness values.



**Figure 12.** Evolution of the conversion efficiency as a function of the electron affinity of the CIGS absorber for various thickness values.

**Figure 12** shows that the efficiency  $\eta$  increases when  $\chi$  goes from 4.0 to 4.2 eV and from 4.6 to 4.8 eV, but declines between 4.2 and 4.6 eV, for all thicknesses (0.1 - 3  $\mu\text{m}$ ). This mirrors the behavior of  $FF$  and  $V_{oc}$ : the central dip is consistent with an increase of  $J_0$  (recombination/leakage) in the less favorable offset region, while the 4.0 - 4.2 and 4.6 - 4.8 eV windows provide a more favorable alignment that enhances  $\eta$  [10] [27].

Partial conclusion. The electron affinity affects  $J_{sc}$  only for ultrathin absorbers (<0.3  $\mu\text{m}$ ), yet it systematically impacts  $V_{oc}$ ,  $FF$ , and  $\eta$ . For good performance,  $\chi \approx 4.0 - 4.2$  eV and  $\chi \approx 4.6 - 4.8$  eV appear favorable [28].

## 5. Conclusions

This study first reviewed the theoretical background and the two-diode equivalent circuit for CIGS cells, together with the governing equations for their electrical parameters. It then detailed the materials, the device structure, and the TCAD methodology used, SILVACO-ATLAS with drift-diffusion transport coupled to Poisson and carrier-continuity equations [7] [8]. Finally, we quantified the impact of the absorber's optical bandgap  $E_g$  and electron affinity  $\chi$  on the figures of merit.

The main findings are as follows:

- 1)  $J_{sc}$  is essentially independent of  $E_g$  over 1.14 - 1.50 eV once the absorber is sufficiently thick ( $\geq 0.3$   $\mu\text{m}$ ); a deviation appears at 0.1  $\mu\text{m}$  (enhanced optical losses), while  $V_{oc}$ ,  $FF$ , and  $\eta$  increase with  $E_g$ .

2) A maximum efficiency of about 27.05% is achieved for  $E_g \approx 1.50$  eV with  $d_{\text{CIGS}} = 3 \mu\text{m}$ , where the rise of  $V_{oc}$  and  $FF$  compensates the near-invariance of  $J_{sc}$ .

3) The electron affinity  $\chi$  affects  $J_{sc}$  only for ultrathin absorbers ( $<0.3 \mu\text{m}$ ); however, it systematically impacts  $V_{oc}$ ,  $FF$ , and  $\eta$ , with favorable windows around  $\chi \approx 4.0 - 4.2$  eV and  $\chi \approx 4.6 - 4.8$  eV across  $0.1 - 3 \mu\text{m}$ .

These trends support the view that joint engineering of  $E_g$  (e.g., via Ga content) and  $\chi$  (band alignment at the CdS/CIGS and TCO interfaces) is a robust lever for optimizing CIGS thin-film solar cells [6] [19] [20] [27] and [28]. In the longer term, a broader comparison with other chalcogenide absorbers (e.g.,  $\text{Sb}_2\text{Se}_3$ ) could refine the performance-sustainability trade-offs highlighted here [29].

## Conflicts of Interest

The authors declare no conflicts of interest regarding the publication of this paper.

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## Abbreviations

**AM1.5G:** Standard solar spectrum (Air Mass 1.5 Global)

**CdS:** Cadmium sulfide (buffer layer, n-type)

**CIGS:** Cu(In, Ga)Se<sub>2</sub>, chalcopyrite absorber (p-type)

**EQE:** External Quantum Efficiency

**FF:** Fill Factor

**IQE:** Internal Quantum Efficiency

**J-V:** Current-density-voltage characteristic

**PET:** Polyethylene terephthalate (substrate)

**PCE:** Power-conversion efficiency

**PLD:** Pulsed Laser Deposition

**STC:** Standard Test Conditions (AM1.5G, 25°C, 1000 W·m<sup>-2</sup>)

**TCAD:** Technology Computer-Aided Design (device simulation)

**TCO:** Transparent conducting oxide

**ZnO:** Zinc oxide (window layer/TCO)

**Mo:** Molybdenum (back contact)

**Al:** Aluminum (front grid/contact)