

Oxidation Behaviour of a Newly Developed Superalloy

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ABSTRACT

The current paper explains the oxidation behaviour of a newly developed nickel-based superalloy in simulating aero gas turbine engine conditions. The results showed that the new superalloy is highly susceptible to high temperature oxidation. Within three of hours of oxidation, extensive oxide scales were formed. The formed oxide scales were analysed with electron dispersive spectroscopy (EDS) and morphology was studied with scanning electron microscope (SEM) for varied oxidation times. The oxidation products were determined with XRD and cross sections of all the oxidised superalloys were also studied. The elemental distribution of all the superalloys after oxidation was also studied with a view to understand and compare the characteristics of the new superalloy with other superalloys. Finally, an oxidation mechanism that is responsible for its faster degradation under elevated temperatures was established based on the results obtained with different techniques and presented in detail.

Keywords: Gas Turbine Engine Components, Superalloys, High Temperature Oxidation

1. Introduction

Newer materials with improved properties are essential in order to enhance the efficiency of gas turbine engines. Efforts made in this direction made it possible to develop a new superalloy for aero engines. The developed superalloy exhibits excellent high temperature strength properties [1]. For achieving enhanced efficiency, it is necessary that the developed superalloy should exhibit excellent high temperature oxidation resistance as it is detrimental at elevated temperatures. It reduces the superalloy component life by forming oxides at a faster rate, thereby reducing the load-carry capacity and potentially leading to catastrophic failure of components. Therefore, high temperature oxidation resistance of new superalloy is as important as its high temperature strength properties.

It is understood that the high temperature capability of superalloys depends on their chemistry such as nature of alloying elements and concentration of each alloying element. The major change is the addition of rhenium or of both ruthenium and iridium at the cost of chromium, which are named as the 3rd or 4th or 5th generation superalloys respectively. Therefore, the chemistry of an advanced superalloy that belongs to 3rd generation was greatly influenced by reducing chromium (Cr) content and increasing the rhenium (Re) content. Similarly, the 4th

and 5th generation superalloys contain only about 3% Cr but instead contain about 6% Re, 1.5% ruthenium (Ru) and/or iridium (Ir), which is a great contrast to the earlier generation superalloys containing about 10% Cr and no Re, Ru or Ir. These are unique elements, which can increase high temperature creep properties considerably, but make the superalloys susceptible to high temperature corrosion *i.e.* hot corrosion and high temperature oxidation. It is due to the fact that the new superalloys cannot form corrosion resistant alumina or chromia scale because of the presence of high rhenium content and small amounts of ruthenium and iridium. Their effect is similar to Mo on oxidation *i.e.* the high vapour pressure of its oxide. Therefore, the new alloying elements are harmful for high temperature corrosion resistance of advanced Ni-based superalloys.

Several failures of gas turbine engine blades were reported during service [2-7]. It was attributed primarily to high temperature corrosion of different types and established their relevant theories. Extensive amount of work was carried out in the laboratory on hot corrosion of several superalloys and established their degradation mechanisms [8-10]. It was shown that the hot corrosion of superalloys takes place through electrochemical reactions and it is an electrochemical phenomenon [10,11]. Further, high performance protective coatings were succ-

essfully identified for protection of superalloys under hot corrosion conditions [12-14]. Efforts made by other researchers in developing protecting coatings helped in understanding their behaviour [15-17]. Basically, the high temperature corrosion can be divided into oxidation and hot corrosion. The hot corrosion can be further divided into type I (800°C - 950°C) and type II (600°C - 750°C). As already mentioned above, any new superalloy material that is developed for gas turbine engine applications should exhibit excellent high temperature corrosion resistance apart from excellent mechanical properties.

In the present paper, high temperature oxidation characteristics of the newly developed superalloy is presented. XRD was used to determine the corrosion products that formed during high temperature corrosion processes. The surface morphologies were studied with scanning electron microscope (SEM) and the composition of oxidation products were analysed by EDS. Elemental distribution of the oxidised superalloys were determined with a view to establish its degradation mechanisms under oxidation conditions.

2. Experimental

The composition of newly developed advanced superalloy is presented in **Table 1**. In contrast to previous generation superalloys, the newly developed superalloy contains 6.5% rhenium and very small content of chromium, which makes it to exhibit very good high temperature strength properties [1]. Disc specimens of about 10 mm diameter and 2 mm thick were cut from the superalloy rods, polished them up to 600 SiC surface finish, cleaned with tap water followed by distilled water and then decreased with acetone. Subsequently, the cyclic oxidation studies were carried out at $1100^{\circ}\text{C} \pm 10^{\circ}\text{C}$ for a period of 100 hours *i.e.* the specimens were placed in a furnace heated at 1100°C for 20 hours and allowed them to cool for 3 hours after removing from the furnace. Initially, the specimens were oxidized only for three hours to determine their weight change and subsequently for every 20 hours. The weight gain measurements were made each time after cooling to room temperature.

After completion of oxidation tests, the specimens were examined for their surface morphology with Scanning Electron Microscope (SEM) and the oxidation products were analyzed by Electron Dispersive Spectroscopy (ED S).

Table 1. The chemical composition of an advanced superalloy (wt%).

Material	Ni	Cr	Co	W	Al	Ta	Re	Hf
New alloy	Bal	2.9	7.9	5.8	5.6	8.5	6.5	0.1

Different phases formed during oxidation were analyzed by X-ray diffraction technique (XRD). Cross sections of oxidized specimens were analyzed for understanding the effect of oxidation and then elemental distribution was determined in order to evolve the degradation mechanisms of advanced superalloy under high temperature oxidation conditions.

3. Results and Discussion

Figure 1 shows as oxidized advanced superalloy. As can be seen, the superalloy was oxidized to a maximum extent by forming thicker oxide scales and subsequently spalled. It indicates that the rate of formation of oxide scales is considerably high on the newly developed superalloy leading to the formation of thick oxide scales over a period of time and subsequently spalled because of adherence problem. In essence, the modified chemistry with increased addition of rhenium and tantalum and considerably reduced chromium made the new superalloy to oxidize at a faster rate when compared to earlier generation superalloys [18]. Typical surface morphology of the oxidized superalloy is shown in **Figure 2**. As can be seen, the surface morphology observed on the alloy is the spalled area as the oxide scale was spalled because of adherence problem due to its high thickness. Almost uniform morphology with reformed oxide scale in some regions is the characteristics of new superalloy. The EDS measurements revealed that the oxide scale was consisted the oxides of base as well as alloying elements. The cross section of oxidized new alloy shows that the oxidation-affected zone is very large (**Figure 3**). Faster oxidation and subsequent spallation is the reason for observing more affected region.

The XRD patterns along with their identifications for the oxidized superalloy after definite oxidation times are demonstrated in **Figure 4** and the oxidation products were summarised in **Table 2**. The superalloy was formed



Figure 1. As oxidised advanced superalloy at 1100°C for 100 hours.

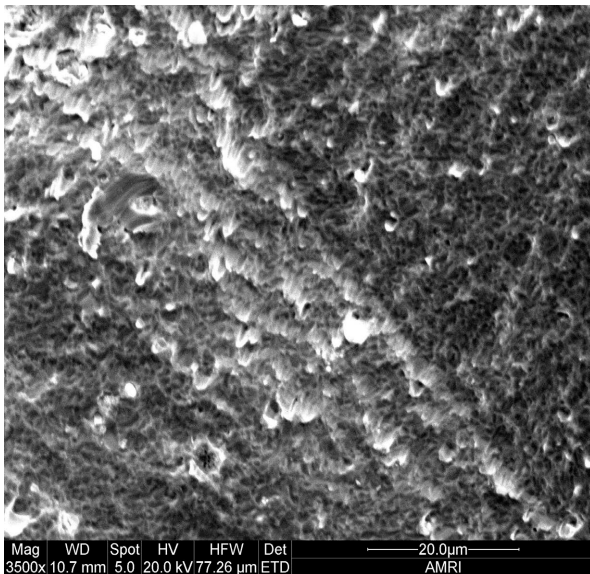


Figure 2. Surface morphology of oxidised superalloy at 1100°C for 100 hours.

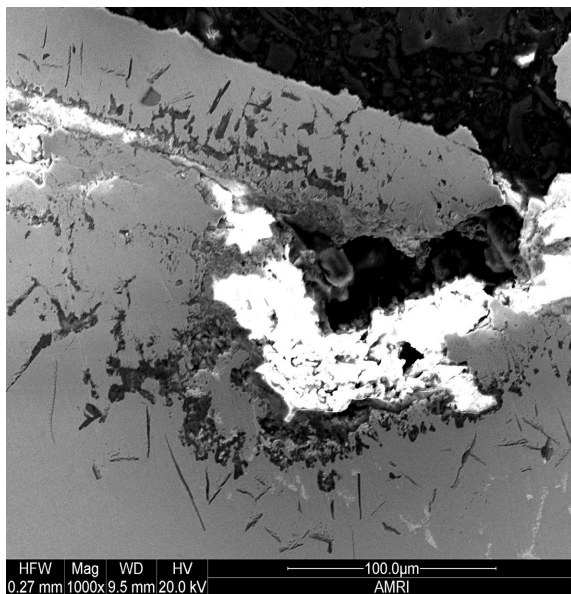


Figure 3. Cross section of oxidised superalloy at 1100°C for 100 hours.

Table 2. XRD data of oxidized superalloy.

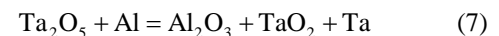
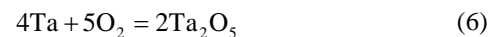
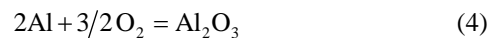
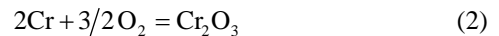
Material	Oxidation products
New superalloy	NiO, Co ₃ O ₄ , TaO ₂ , WO ₃ , Al ₂ O ₃

nickel oxide as well as oxides of all the alloying elements (**Table 2**) during high temperature oxidation. The dominant oxidation product was nickel oxide with small peaks

relating to oxides of cobalt, tantalum, tungsten and aluminium. It is due to the fact that the oxide scale was spalled because of high thickness.

The elemental distribution of an advanced superalloy after oxidation at 1100°C for 100 hours is illustrated in **Figure 5**. Discontinuous alumina in association with chromia is clearly observed on its surface. Rhenium and cobalt were present beneath the alumina and chromia scale. No nickel and cobalt oxides were present. These oxides might have spalled during cutting and polishing, as they are prominent in XRD. It demonstrates that the external scale was consisted of nickel and cobalt oxides, which were spalled after attaining maximum thickness and the internal scale was a mixture of alumina, chromia and tantalum oxide and hence observed in the cross section.

The present investigation clearly established that the newly developed superalloy is highly vulnerable to high temperature oxidation and degrades due to formation of a multilayer corrosion products consists of oxides of nickel as well as the alloying elements. During normal oxidation of superalloys, the oxides of most of the alloying elements as well as base are expected to form as given below:



Due to reaction with oxygen, rapid weight gain of the alloys takes place initially. After oxidation for an appropriate time, thermodynamically stable oxides such as Al₂O₃, Cr₂O₃ are formed as a dense oxide scale on the surface of superalloys. These oxide scales act as diffusion barriers for the ingress of deleterious species such as oxygen and sulphur. However, the oxidation is significantly high for the new superalloy, as it could not able to form a stable alumina or chromia scale because of change in its chemistry.

The following degradation mechanism has been proposed for the oxidation of new superalloy: diffusion processes occurring at elevated temperatures at the superalloy and environment interface act as a major degradation

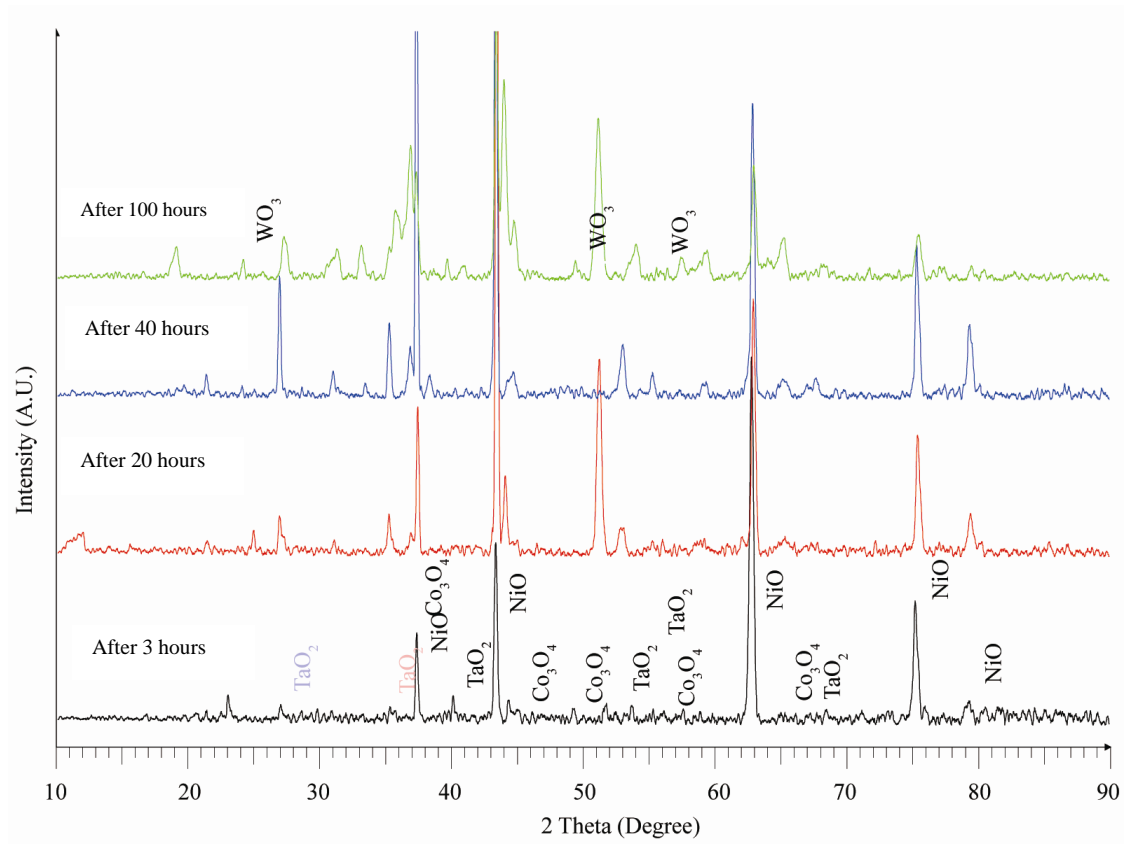


Figure 4. XRD Patterns of an advanced superalloy after oxidation at 1100°C for different times.

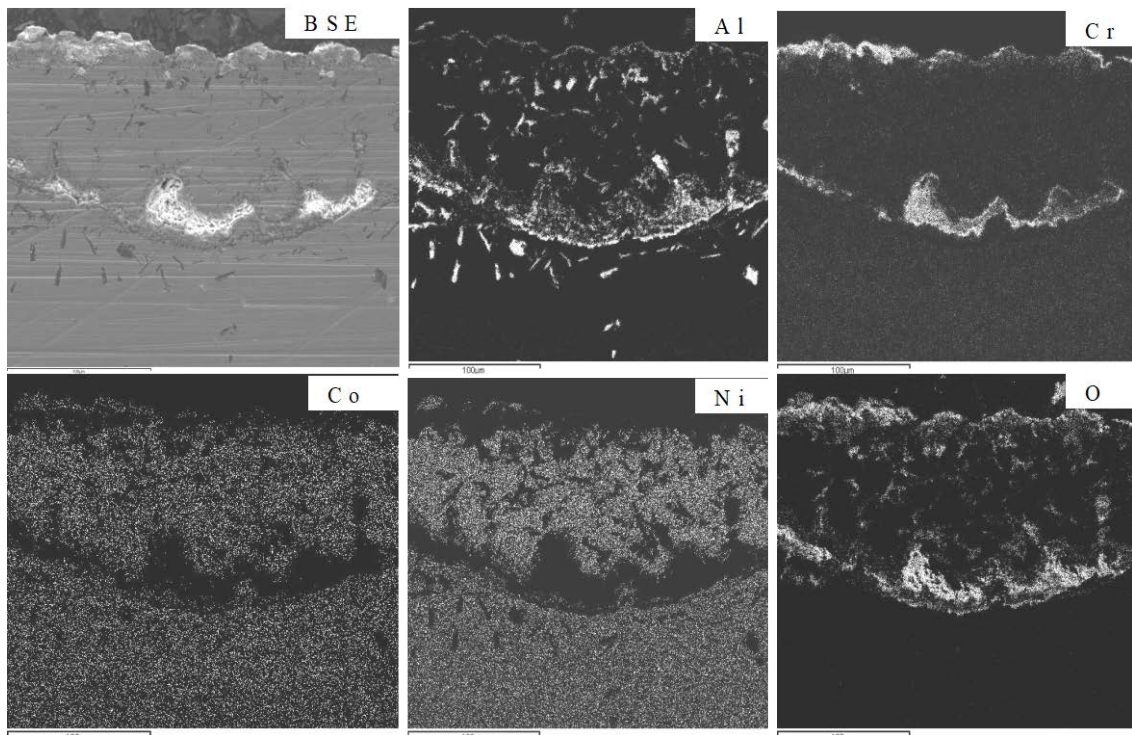


Figure 5. Elemental distribution of an advanced superalloy after oxidation at 1100°C for 100 hours.

mode of the superalloy. At the superalloy interface, diffusion occurs primarily due to thermodynamic considerations at the elevated temperatures. The new superalloy contains a number of alloying elements like Co, Ta, W, Re, Al, Cr etc. mainly to enhance high temperature mechanical characteristics. The nickel and alloying elements of the superalloy diffuse outwards leading to the formation of phases that contain non-protective elements during high temperature oxidation process. As a result, non-protective oxide scales form rather than continuous and protective pure alumina scale. It is important to mention that nickel appears to have high affinity towards oxygen at elevated temperatures and hence diffuses outwards at a faster rate, interact with oxygen ions to form nickel oxide. This process leads to extensive nickel oxide growth and forms thicker scales. Thicker scales lead to spall after reaching to certain thickness due to adherence problem. Further, excessive growth of nickel oxide scale, in association with alloying elements of superalloy like cobalt, tantalum, tungsten and rhenium, leads to the formation of non-protective oxide scales with large volumes. Consequently, spallation of oxide scale takes place because of non-adherence to the superalloys. Practical observation of extensive oxide scale growth (Figure 5) and subsequent spallation clearly supports the proposed degradation mechanism. A schematic representation of degradation of new superalloy during high temperature oxidation is presented in Figure 6.

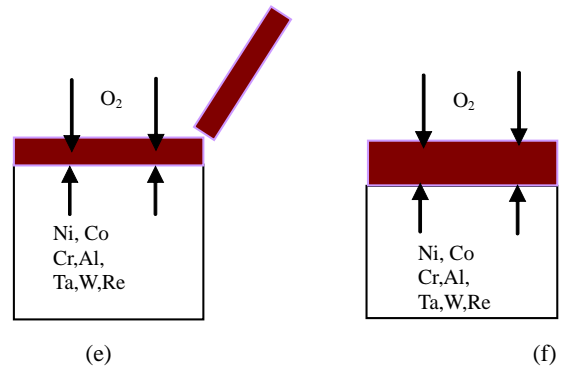
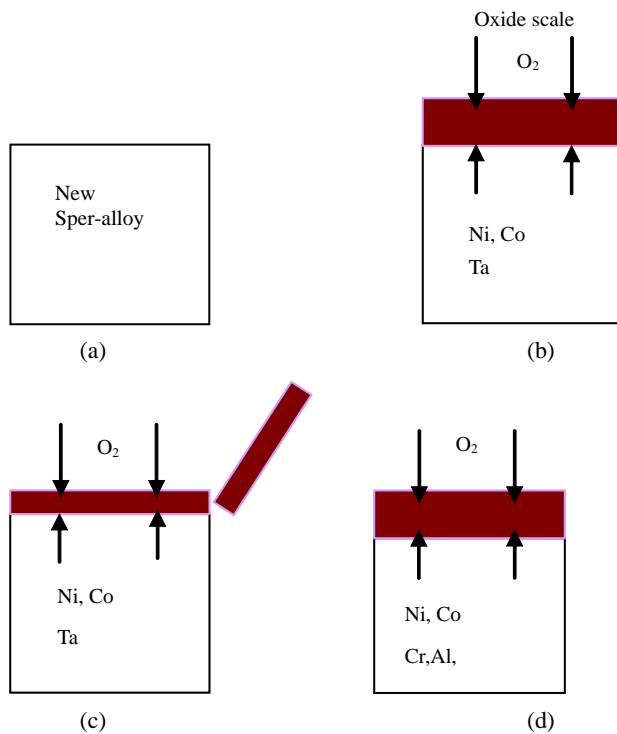


Figure 6. Sequence of degradation processes for an advanced superalloy during high temperature oxidation process. (a) Before oxidation; (b) During 3 hours of oxidation; (c) After 3 hours of oxidation; (d) During 20 hours of oxidation; (e) After 20 hours of oxidation; (f) After 40, 60, 80, 100 hours of oxidation and continuation of process leading to failure of the alloy.

4. Development of Smart Coatings

The present results clearly stress the need to apply high performance protective coatings for its protection against high temperature oxidation as the gas turbine engines encounter oxidation problem during service. The protective coatings allow the gas turbine engines to operate at varied temperatures and enhance their efficiency by eliminating failures during service. Research in this direction has resulted in design and development of smart coatings which provide effective protection to the superalloy blades for the designed period against type I, type II hot corrosion and high temperature oxidation that are normally encountered in gas turbine engines which in turn enhances the efficiency of gas turbine engines considerably [18,19]. This is a major developmental work in the area of gas turbine engines used in aero, marine and industrial applications. Unlike the conventional/existing coatings, the smart coatings provide total protection to the superalloy components used in aero, marine and industrial applications by forming appropriate protective scales depending on the surrounding environmental conditions [18, 19].

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